
H8/300

Using a H8/300 to control a stepper motor

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Introduction

The H8/300 family of microcontrollers are multi-purpose, 8-bit data path devices used in a multitude of applications that require a low-cost controller with adequate performance and a high mix of peripheral integration. In particular, versatile timer modules with built-in comparators and capture functions able to run at various frequencies are needed in virtually most control applications. All H8/300 family members possess a 16-bit free-running counter used primarily to generate various frequency and duty-cycle rectangular waveforms through its 2 output channels. Even if an application requires more than 2 control output signals, the timer can still be utilized in determining the pulse width of the output waveforms, while the signals can be generated at various I/O lines. An example of such situations can be found in various motion control applications that require multiple phase excitation waveforms for activation.

In general, a variety of alternatives are available for motion control, such as linear and rotary solenoids, servo motors, AC and DC motors, and stepper motors. For applications that require accurate positioning and moderate positioning speed at a reasonable cost, a stepper motor implementation is the ideal choice. Such applications range from printers to tape drives, floppy disc drives, medical instrumentation, robotics equipment, and other digitally controlled positioning systems.

This application note will show how an H8/330 can be utilized to control the operation of a stepping motor. Although the H8/330 was the chosen device, any member of the H8/300 Family could be used in the process (with the obvious exception of the H8/310 and H8/3101 that lack a timer module). A simple motion control embedded system can be designed utilizing only a H8/330 controller, a stepper motor, and the motor-specific required control circuitry (consisting of power FET transistors, clamping diodes, and current-limiting high-power resistors).

Using a H8/300 to control a stepper motor

Stepper Motor Characteristics

Before stepping into the design example, a brief synopsis of a stepper motor features is warranted. Figure 1 depicts an example of how a simple, 2-phase stepper motor is built. It consists of a disc centered and mounted on a shaft which is free to rotate between a pair of stator poles. The disc consists of a series of permanent magnets radially distributed on its surface. Two electromagnetic coils are wound around each stator pole. Energizing the coils with the proper polarities will generate a magnetic field pattern to which the permanent magnets on the rotor disc will try to align producing a torque. As a result, the disc will rotate until the stator poles are aligned with the next permanent magnet, hence taking a "step". The numbers of radial permanent magnets on the disc determine the stepping angle of the rotor, hence the number of steps.

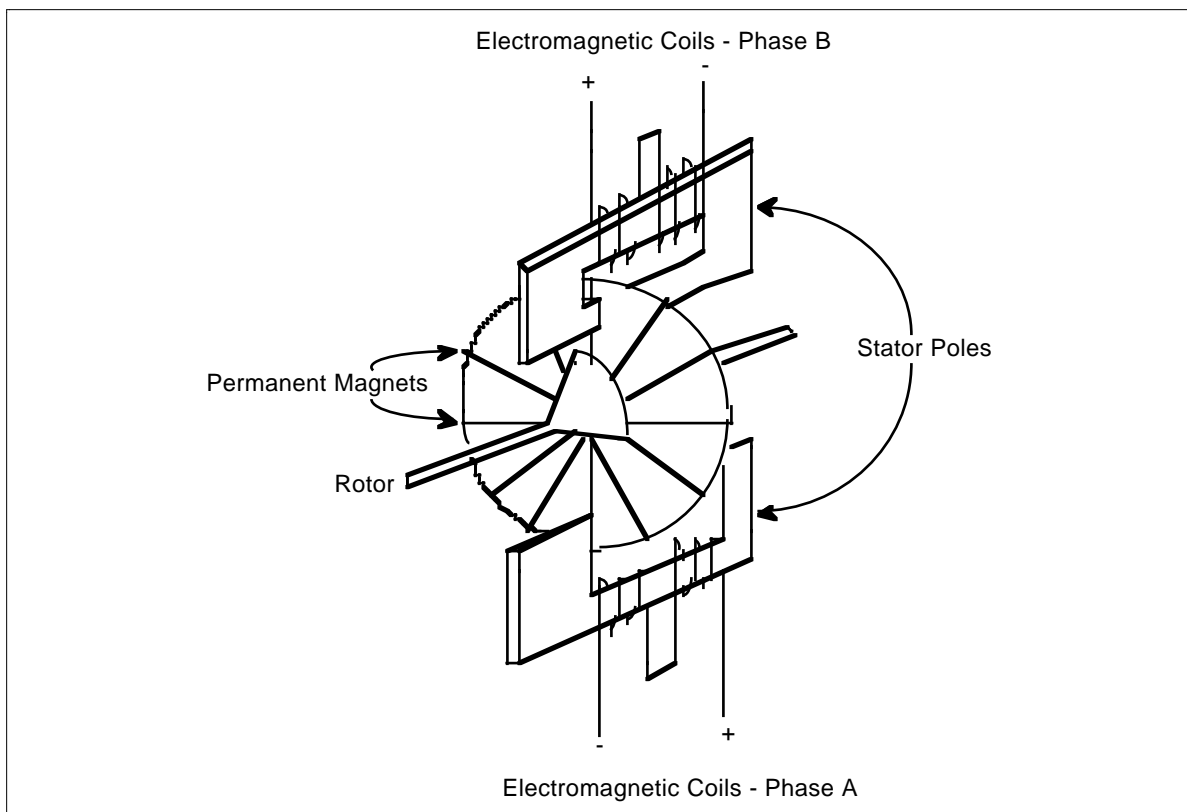


Figure 1

The electromagnetic coils in figure 1 must be energized in a particular fashion in order to allow the rotor to take incremental steps. The voltage drop across each coil determines how fast the current will build in the coil windings, hence the speed of the motor. An example of the needed circuitry in order to provide alternating voltage drops across the electromagnetic coils is shown in figure 2.

Using a H8/300 to control a stepper motor

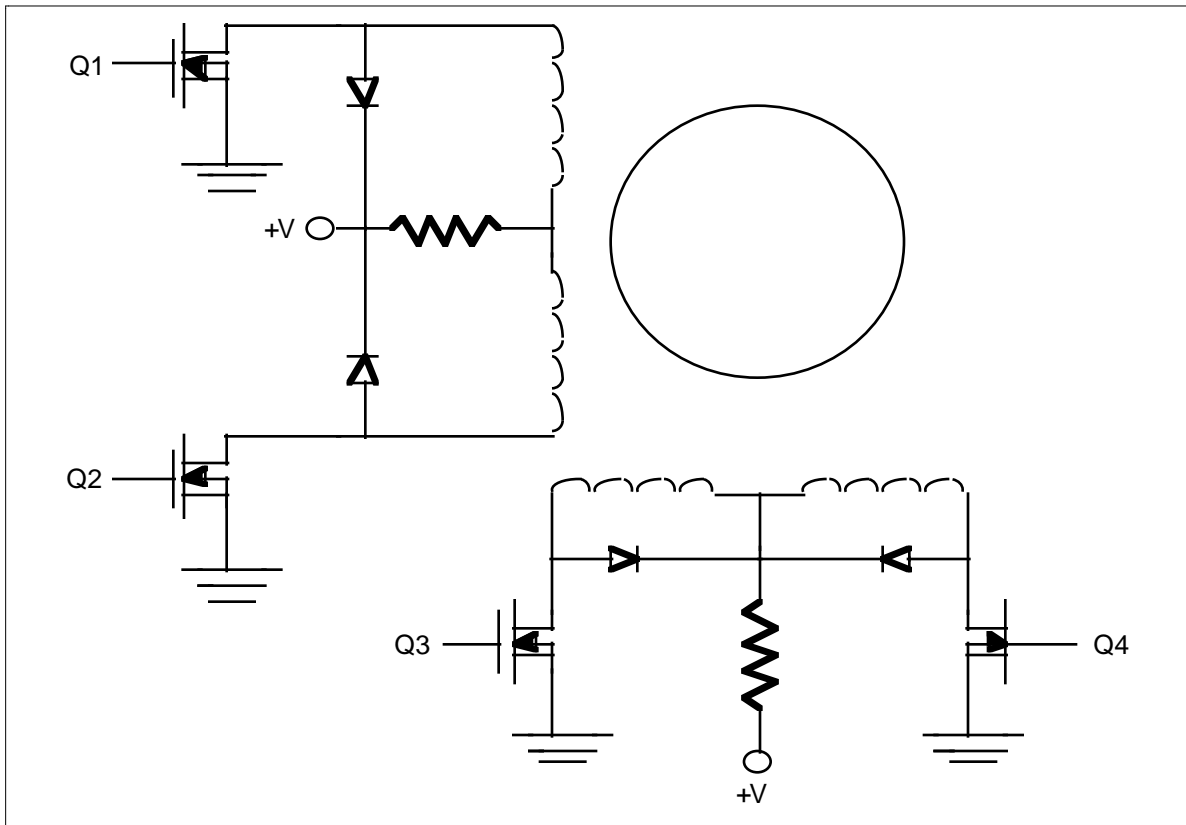


Figure 2

In order to cause the motor shaft to rotate in a clockwise fashion one step at a time, the 4 MOSFET transistors must be turned on and off in the 4 step sequence shown in table 1 below. For constant step rotation, this sequence must be repeated continuously.

Table 1

Step	Q1	Q2	Q3	Q4
1	On	Off	On	Off
2	On	Off	Off	On
3	Off	On	Off	On
4	Off	On	On	Off

For counterclockwise rotor motion, the step sequence shown above must simply be reversed. The resistors in figure 2 provide coil protection by limiting the current to the specified maximum in accordance with the motor specifications. The 4 clamp diodes prevent the voltage across the inductive winding to reach levels that would damage the MOSFET switching transistors as they are turned off. The speed of the motor depends upon 2 factors: the +V voltage level and/or the time this voltage is applied at the coils.

First, we consider the voltage level. Applying a voltage at the +V point will produce a current flow through the coils if the corresponding transistor is biased. However, due to the coil inductance, the current will

Using a H8/300 to control a stepper motor

reach its steady state value in a finite time; its value will depend upon the motor winding series resistance, the coil inductance, and the applied voltage, according to the formula:

$$i(t) = V/R(1 - e^{-R/L})$$

Figure 3 shows how this current is built up as a function of time for different voltage values. The higher the voltage, the quicker the current will build up and reach its steady value, and the faster the rotor will move to the next step position.

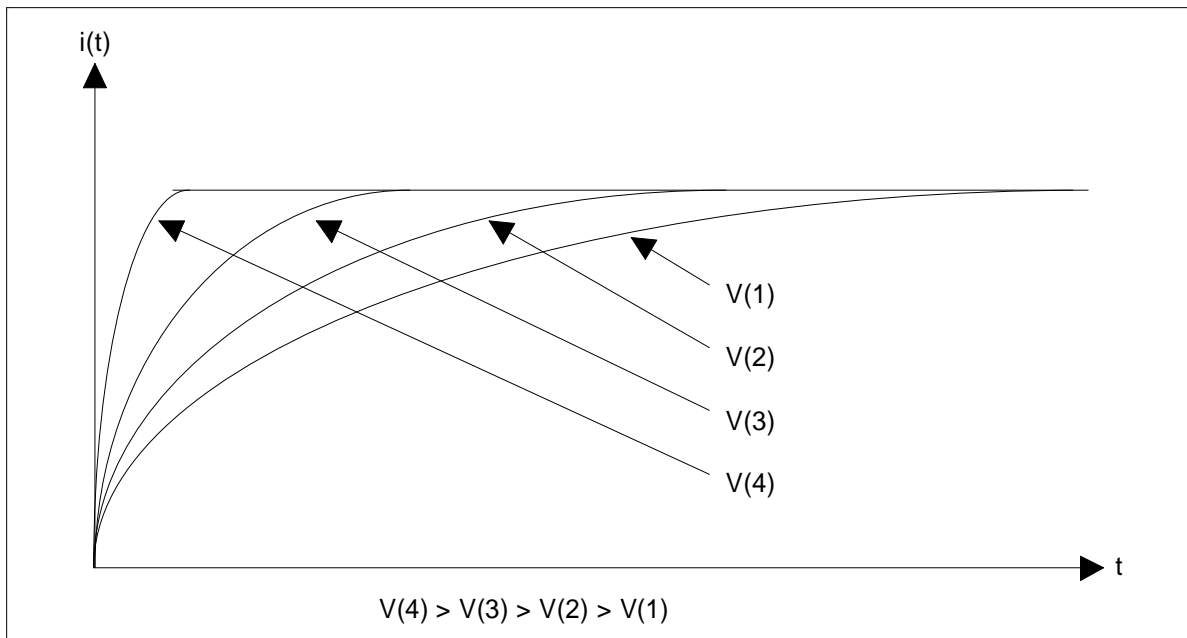


Figure 3

Second, we consider the time the voltage is applied at the electromagnetic coils. As mentioned above, the +V voltage will create a steady state current as long as the transistor associated with the coil is turned on. The shorter the MOSFETs are active for each step shown in figure 3, the quicker will the motor go through each step. Therefore, by successively decreasing the active time of the MOSFETs, the motor performs an accelerated rotational motion. Vice versa, as the transistors active time is gradually increased, the motor will decelerate. Of course, there is a minimum active time and voltage that must be supplied in order for the motor to properly rotate, and it depends upon the motor torque characteristics. Figure 4 shows the alternating states of the 4 transistors in order to perform the motor full-stepping process.

Using a H8/300 to control a stepper motor

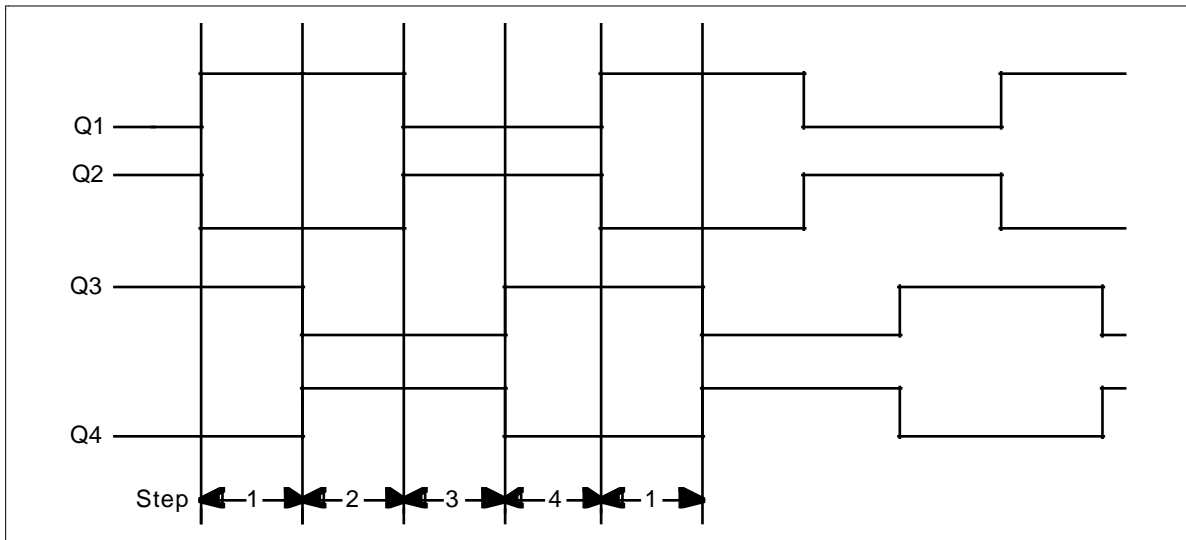


Figure 4

These excitation waveforms correspond to a 2-phase 4 excitation process. The input at Q1 corresponds to phase A, the Q3 input to phase B, the Q2 input to the inverse of phase A, and the input at Q4 to the inverse of phase B. Since phase A falls while phase B is low, figure 4 depicts the excitation waveforms for a clockwise (CW) motion. For counter clockwise (CCW) rotation, phase A must fall while phase B is high.

As a final aspect to be considered, each stepper motor, being a mechanical device, has limitations on how much current can be supplied to the coils and for how long in order for the shaft to rotate each step. A typical relationship between the motor torque, current and the stepping rate (in pulses per second) is shown in figure 5. In order to overcome inertia, the motor must be supplied a minimum amount of current in order to take one step. During continuous stepping with a constant voltage supply, the dynamic torque developed decreases with increasing stepping rate. There is also a maximum stepping rate to which the motor will respond; overdriving this rate will cause rotor vibration and no stepping will be performed.

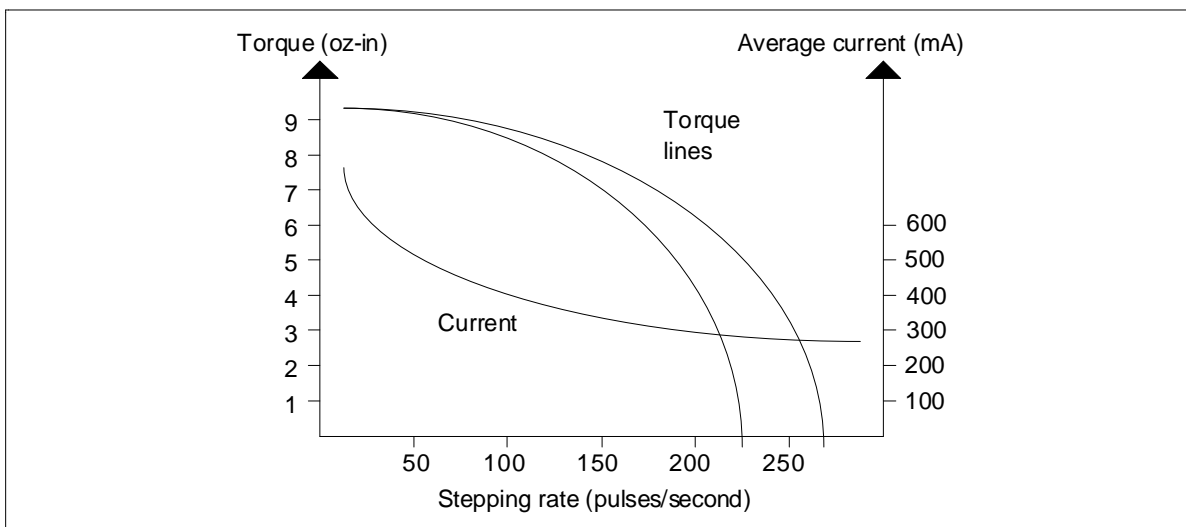


Figure 5

Using a H8/300 to control a stepper motor

Design Example

As stated in the introduction, the H8/330 microcontroller is utilized to provide the stepper motor control waveforms. The stepper motor used required 2-phase 4 excitation waveforms, and was of a so-called bifilar type. This term refers to the type of windings used in the 2 stator coils; specifically, bifilar windings contain 2 coils in each stator half. It is important to note that although a bifilar-wound motor contains 4 coils (or phases), it is essentially operated as a 2-phase motor. The motor used is manufactured by Hitachi, Ltd. and it is of a permanent magnet type; its part number is KP6P8-701. Appendix A shows its standard specifications and its torque-versus-pulse rate curve measured at an excitation voltage of +12V.

The hardware utilized for this project consisted of the following main parts:

1. The H8/330 evaluation board.
2. A specially wire-wrapped motor interface circuitry board used to boost the motor control signals, and provide the motor power supply requirements.
3. The KP6P8-701 permanent-magnet stepper motor.

The H8/330 is supplying the initial 4 excitation waveforms via the 4 I/O output lines P8₃ - 6. P8₃ produces the phase A waveform, P8₄ the phase B waveform, P8₅ the inverted phase A waveform, and P8₆ the inverted phase B waveform. The motor interface board schematic is shown in figure 6. The initial motor excitation signals are driven through AND gates, and are available as long as 5V power is supplied to the system. Next, they are input to the gates of 4 MOSFET transistors (type 2SK1095), alternately switching them on and off. These transistors act as a drain for the current generated across the electromagnetic coils of the motor. Four protection diodes of the type HRP-22 are used to keep the voltage drop between the drain and the source to 0.55V. Finally, power is supplied to the motor windings from a +12V power supply through a pair of low-resistance, high power dissipation loads. Figure 7 shows the waveform output from the H8/330 in order to produce successive motor steps. Since the MOSFET's switching time is extremely fast (50-400ns depending upon the drain current), a dead-time (t) is inserted between inverting phase signals (A and A-, B and B-) so that A- and B- go low a little bit before A and B are turned on.

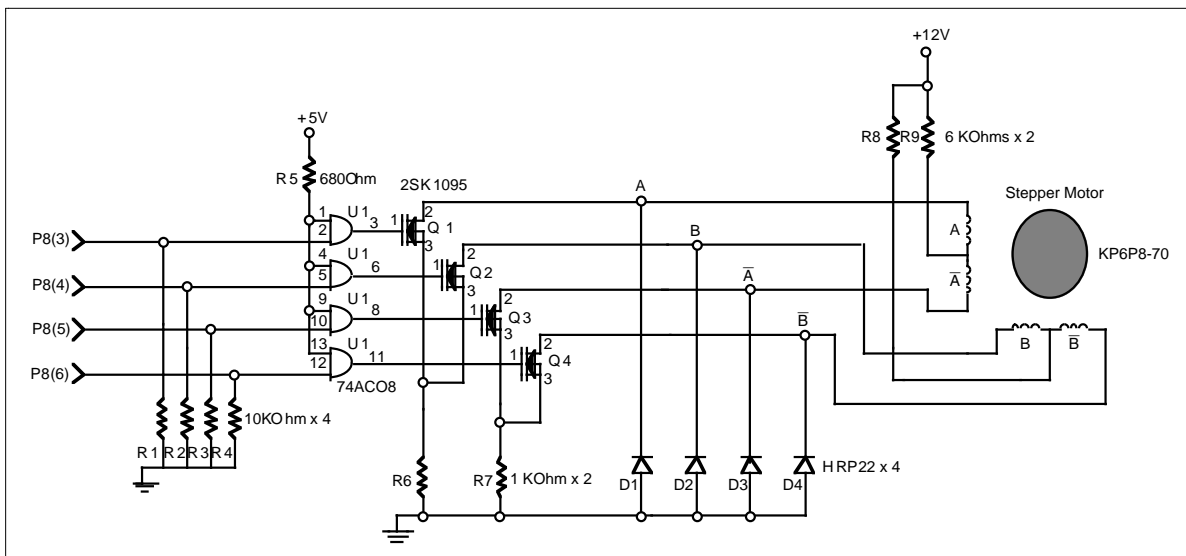


Figure 6

Using a H8/300 to control a stepper motor

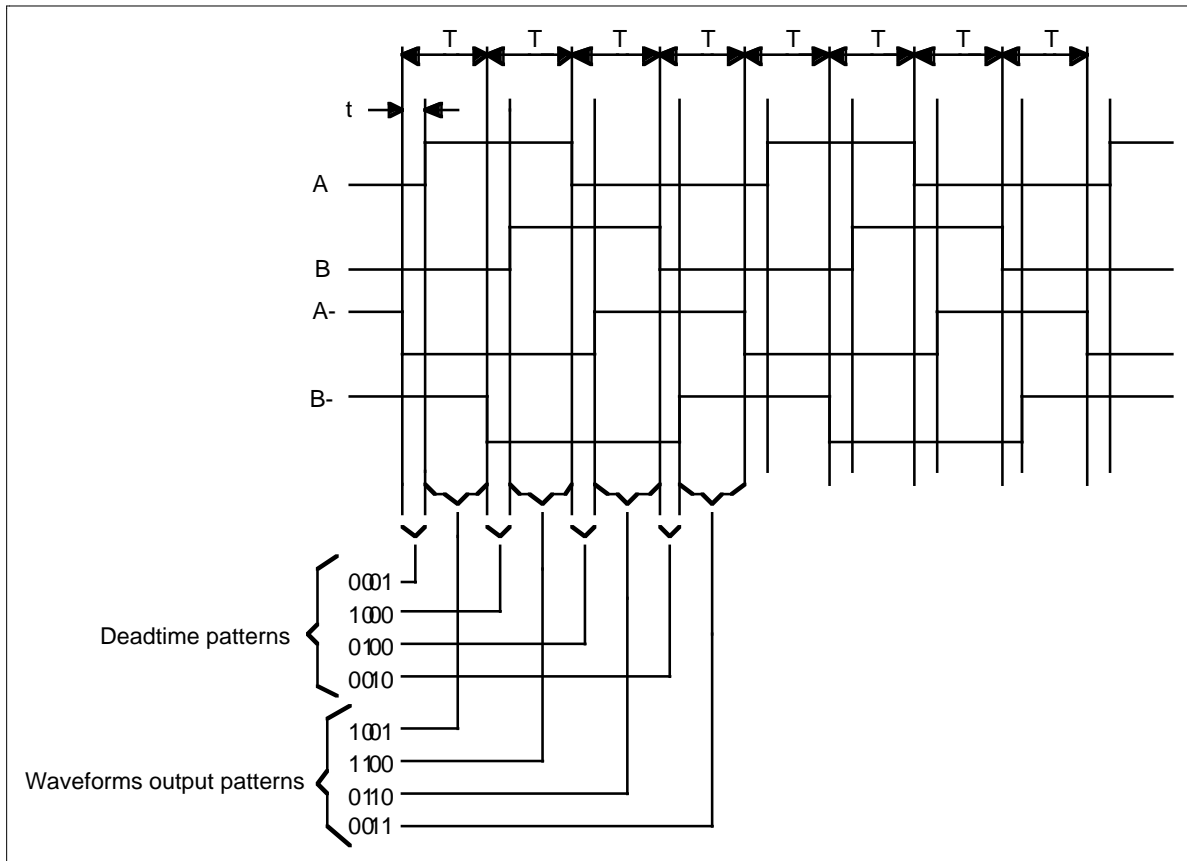


Figure 7

If the stepper motor is driven with the waveforms depicted in figure 7, a constant clockwise stepping motion is generated. If the waveform period T is less, the motor will step through quicker, while if it is longer, so will be the stepping intervals. If T is gradually decreased, the shaft will perform an accelerated rotational motion, while if it is increased, it will decelerate. The full-stepping clockwise sequence corresponds to the 4 data patterns shown on the bottom left in figure 7.

This operation is implemented by using the 16-bit free-running timer of the H8/330 to time out via the P8₃₋₆ output-configured pins the waveform pattern shown in figure 7. The A comparator inside the timer module alternatively holds the timer counts corresponding to the non-overlap and excitation times. The first non-overlap pattern time and the first excitation pattern time are output as a result of polling the output-compare A flag. The next non-overlap pattern is output when a compare-match A interrupt occurs, and the next excitation pattern time is issued by polling when the compare-match A flag is set. This process then continues ad infinitum and is illustrated in Figure 8.

Using a H8/300 to control a stepper motor

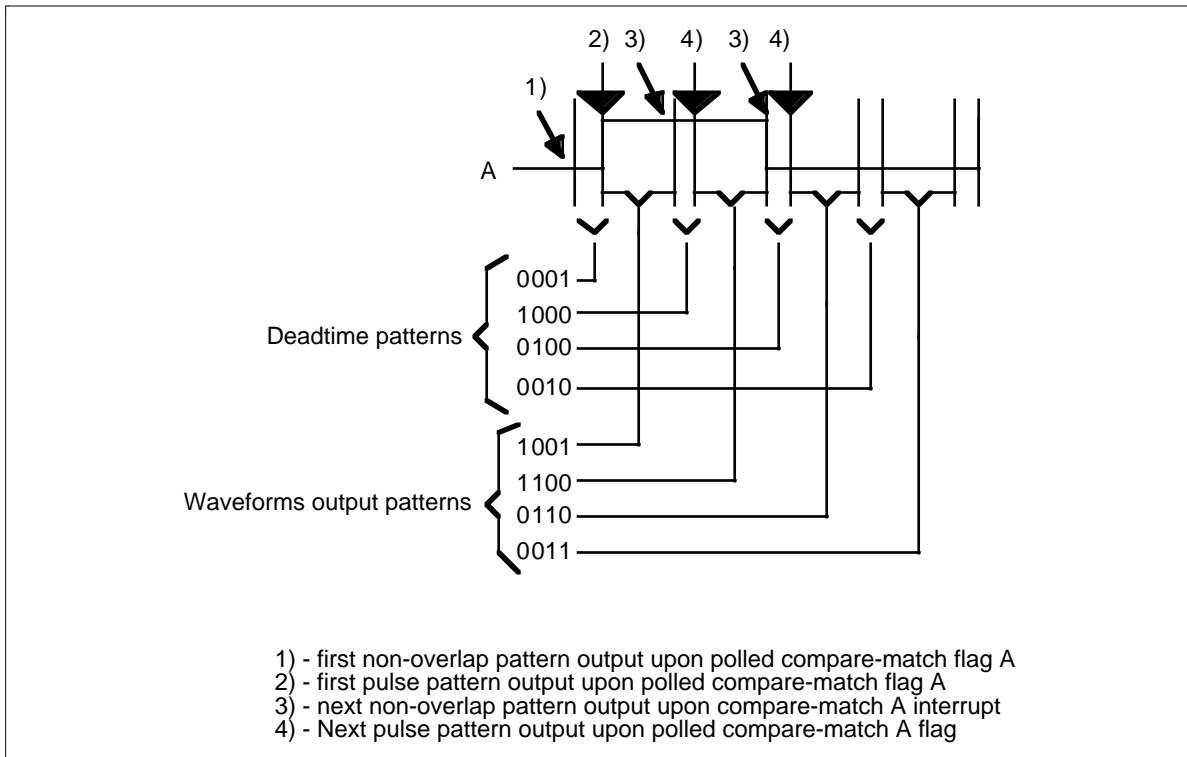


Figure 8

Using a H8/300 to control a stepper motor

Software Description

The code controlling the process explained in the previous section consists of 4 main parts:

1. The non-overlap and excitation pattern look-up table.
2. Initializations of CPU, constants, I/O Port, and 16-bit timer.
3. The first 2 loops that control the timing of the first non-overlap and excitation patterns.
4. The compare-match A interrupt service routine that provides the timing for the next non-overlap and excitation patterns.

The look-up table consists of 8 hexadecimal values corresponding to the 4 excitation waveforms patterns. The 4 non-overlap patterns alternate with the 4 pulse patterns.

After the CPU is initialized, 4 constant values that are to be used later in the program are initialized. The non-overlap time count and the pulse output time count are stored in R1H and R2 respectively. These values are loaded into the Output Compare Match Register A (OCRA) of the 16-bit Free Running Counter Timer. R3L contains the pattern count corresponding to the number of output patterns that repeat in a cycle (8). R1L contains the initial count that starts up the whole process.

The 16-bit timer is set to clear the contents of the free-running counter register (FRC) when a compare-match between OCRA and FRC occurs. Also, the timer clock is set to $\Phi/8$. The I/O Port 8 data direction register (P8DDR) is configured for outputs only, and the data register (P8DR) is cleared.

The process starts by loading the startup count into the OCRA, and polling the compare-match A flag (OCFA) until it is set. Then, the first value in the look-up table (corresponding to the first non-overlap pattern) is output at the I/O Port 8_{3-6} lines. The OCRA is loaded with the non-overlap count value in R1H, the OCFA flag is cleared, and the pattern count in register R3L is decremented. The next loop polls the OCFA flag again, and upon flag set, the first pulse output pattern is output. Next, the OCRA is updated with the pulse count value in R2, OCFA is cleared, the pattern count R3L decremented, and the output-compare interrupt A enable flag (OCIAE) in the Timer Interrupt Enable Register (TIER) is set. The program then enters an infinite loop that basically waits for the interrupt to occur.

The interrupt routine is serviced when the contents of OCRA match the contents of FRC. Then, the next non-overlap pattern is output at the $P8_{3-6}$ lines, the OCRA is updated, the OCIAE and OCFA flags are cleared, and the pattern count is decremented. Loop 3 within the interrupt service routine polls the OCFA flag, and upon compare-match, the next pulse pattern is output. If the pattern count is not zero, the OCRA is loaded with the pulse count, the OCIAE is set, and the program exits the interrupt service routine and enters the wait loop again. If the pattern count is 0, the first pattern in the look-up table is loaded again and the process continues. Figures 9 and 10 show the main program and the interrupt service routine flowcharts. The program listing follows the flowcharts.

Using a H8/300 to control a stepper motor

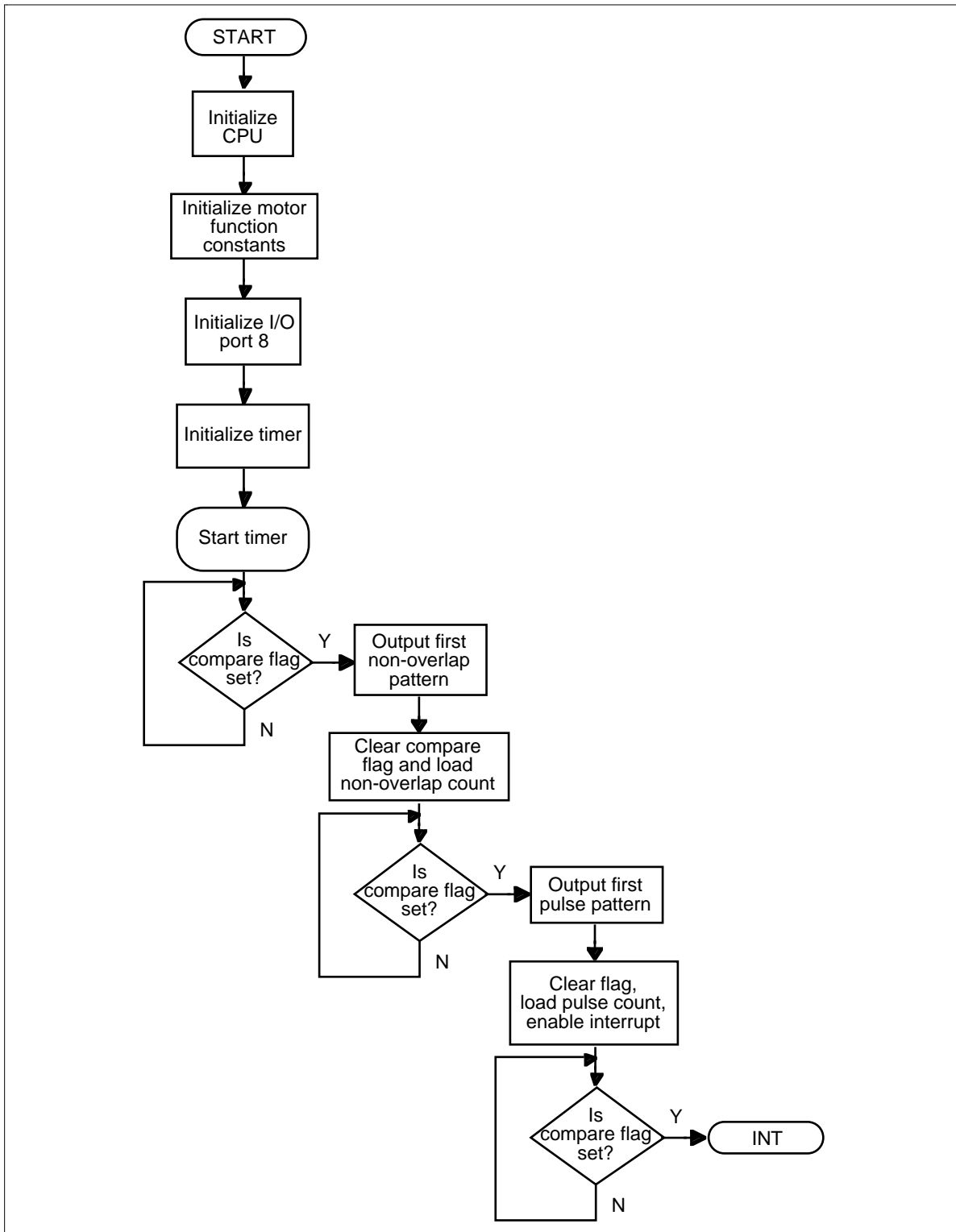


Figure 9

Using a H8/300 to control a stepper motor

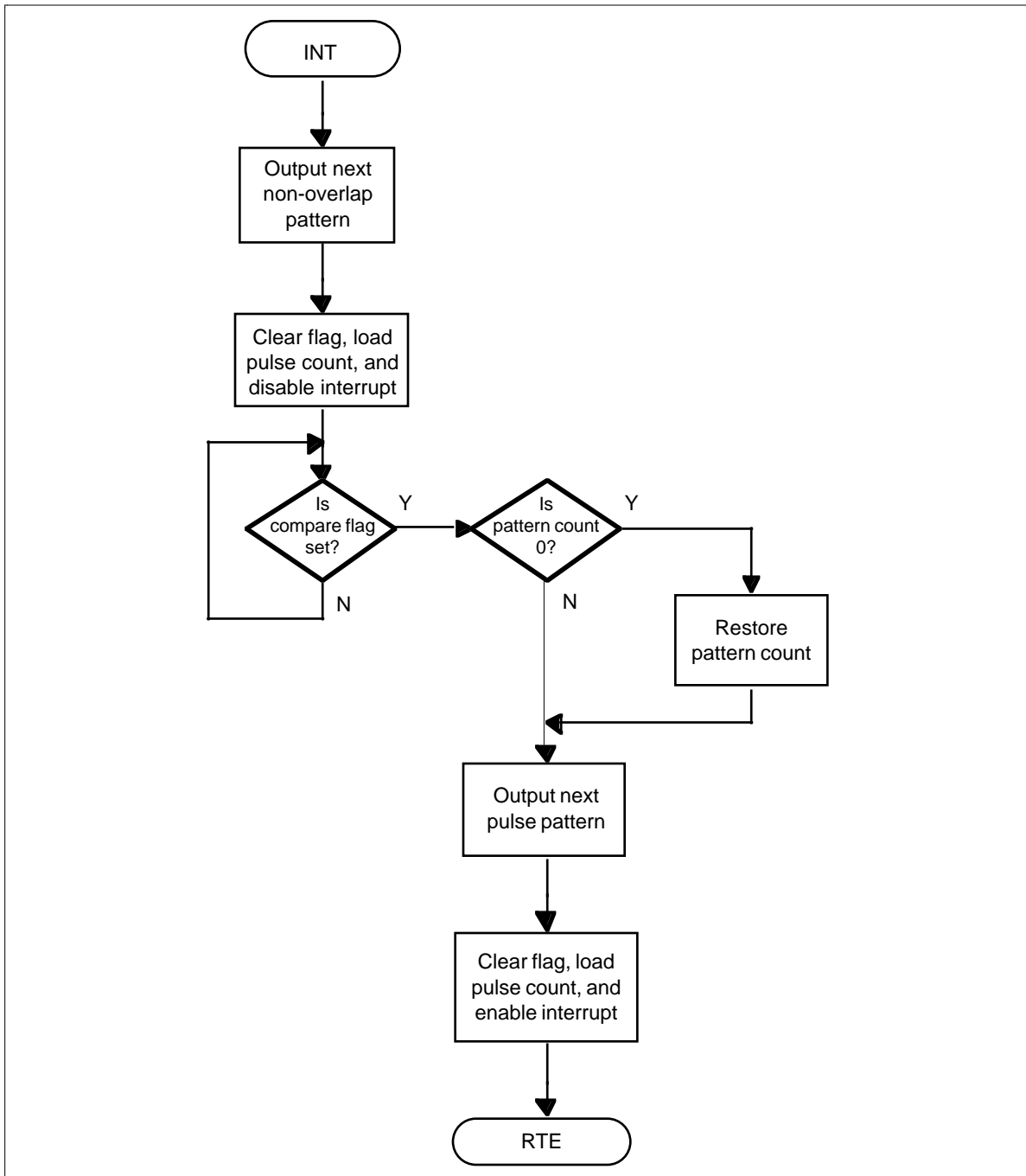


Figure 10

Using a H8/300 to control a stepper motor

Program listing - motor.lst

Microtec Research ASMH83 Version 1.0A Sep 08 11:11:35 1994 Page 1

Command line: C:\MRI\ASMH83\ASMH83.EXE -l m2.src

```
Line      Addr
1         FF90          TIER   .EQU   H'FF90
2         FF91          TCSR   .EQU   H'FF91
3         FF92          FRC    .EQU   H'FF92
4         FF94          OCRA   .EQU   H'FF94
5         FF96          TCR    .EQU   H'FF96
6         FF97          TOCR   .EQU   H'FF97
7         FFBD          P8DDR  .EQU   H'FFBD
8         FFBF          P8DR   .EQU   H'FFBF
9
10                .ORG   H'0020
11         0020 025C          .DATA.W INT
12
13                .ORG   H'100
14         0100 88C8 C0E0          .DATA.B H'88,H'C8,H'C0,H'E0
15         0104 A0B0 9098          .DATA.B H'A0,H'B0,H'90,H'98
16
17                .ORG   H'200
18         0200 7907 FF80          START: MOV.W  #H'FF80,R7      ;SET
STACKPOINTER
19         0204 0700          LDC    #0,CCR
20         0206 7906 0100          MOV.W  #H'100,R6      ;POINT TO
OUTPUT PATTERN MEMORY TABLE
21         020A F9FF          MOV.B  #H'FF,R1L     ;STARTUP
COUNT
22         020C F11F          MOV.B  #H'1F,R1H     ;NON-OVERLAP
COUNT
23         020E 7902 0800          MOV.W  #H'0800,R2    ;PULSE COUNT
24         0212 FB08          MOV.B  #H'08,R3L     ;PATTERN
COUNT
25
26                ;      I/O PORT 8 SETUP
27
28         0214 F8FF          MOV.B  #H'FF,R0L     ;PORT 8 IS
OUTPUT
29         0216 38BD          MOV.B  R0L,@P8DDR
30         0218 F800          MOV.B  #H'0,R0L
```

Using a H8/300 to control a stepper motor

```

31          021A 38BF          MOV.B   R0L,@P8DR
32
33          ;          TIMER INITIALIZATION
34
35          021C F801          MOV.B   #H'01,R0L          ;CLEAR FRC
AT COMPARE-MATCH A
36          021E 3891          MOV.B   R0L,@TCSR
37          0220 3896          MOV.B   R0L,@TCR          ;TIMER CLOCK
IS /8
38
39          ;          START TIMER WITH STARTUP COUNT
40
41          0222 3994          MOV.B   R1L,@OCRA
42          0224 7900 FFFF          MOV.W   #H'FFFF,R0
43          0228 6B80 FF92          MOV.W   R0,@FRC
44          022C 7E91 7330          LOOP1:  BTST.B  #3,@TCSR          ;STARTUP
LOOP
45          0230 47FA          BEQ     LOOP1
46          0232 6C6D          MOV.B   @R6+,R5L          ;OUTPUT
FIRST NON-OVERLAP PATTERN
47          0234 3DBF          MOV.B   R5L,@P8DR
48          0236 1A0B          DEC     R3L
49          0238 3194          MOV.B   R1H,@OCRA          ;LOAD OCRA
W/ NON-OVERLAP COUNT
50          023A 7F91 7230          BCLR.B  #3,@TCSR          ;CLEAR
COMPARE-MATCH FLAG
51          023E 7E91 7330          LOOP2:  BTST.B  #3,@TCSR          ;FIRST NON-
OVERLAP LOOP
52          0242 47FA          BEQ     LOOP2
53          0244 6C6D          MOV.B   @R6+,R5L          ;OUTPUT
FIRST PULSE PATTERN
54          0246 3DBF          MOV.B   R5L,@P8DR
55          0248 1A0B          DEC     R3L
56          024A 6B82 FF94          MOV.W   R2,@OCRA          ;LOAD OCRA
W/ PULSE COUNT
57          024E 7F91 7230          BCLR.B  #3,@TCSR          ;CLEAR
COMPARE-MATCH FLAG
58          0252 7F90 7030          BSET.B  #3,@TIER          ;ENABLE
COMPARE-MATCH INTERRUPT
59          0256 40FE          WAIT:  BRA     WAIT          ;WAIT FOR
INTERRUPT
60          0258 0000          NOP
61          025A 0000          NOP
62

```

Using a H8/300 to control a stepper motor

```
63                                ;      INT INTERRUPT SERVICE ROUTINE
64
65      025C 1A0B                  INT:   DEC      R3L
66      025E 6C6D                  MOV.B  @R6+,R5L      ;NEXT NON-
OVERLAP OUTPUT
67      0260 3DBF                  MOV.B  R5L,@P8DR
68      0262 3194                  MOV.B  R1H,@OCRA    ;NON-OVERLAP
COUNT
69      0264 7F90 7230            BCLR.B #3,@TIER     ;DISABLE
INTERRUPT
70      0268 7F91 7230            BCLR.B #3,@TCSR     ;CLEAR
COMPARE-MATCH FLAG
71      026C 7E91 7330            LOOP3: BTST.B #3,@TCSR ;NON-OVERLAP
LOOP
72      0270 47FA                  BEQ    LOOP3
73      0272 1A0B                  DEC    R3L
74      0274 4606                  BNE    CONT
75      0276 FB08                  MOV.B  #H'08,R3L    ;RESTORE
PATTERN COUNT
76      0278 7906 0100            MOV.W  #H'100,R6    ;POINT TO
START PATTERN AGAIN
77      027C 6C6D                  CONT:  MOV.B  @R6+,R5L ;NEXT PULSE
OUTPUT
78      027E 3DBF                  MOV.B  R5L,@P8DR
79      0280 6B83 FF94            MOV.W  R3,@OCRA    ;LOAD OCRA
W/ PULSE COUNT
80      0284 7F91 7230            BCLR.B #3,@TCSR     ;CLEAR
COMPARE-MATCH FLAG
81      0288 7F90 7030            BSET.B #3,@TIER     ;ENABLE
COMPARE-MATCH INTERRUPT
82      028C 5670                  RTE
83                                .END
```

Using a H8/300 to control a stepper motor

Appendix A - Motor Standard Specifications

Model	KP6P8
Phase	4
Step Angle (degrees/step)	7.5
Voltage (V)	12
Current (Amps/phase)	0.33
Resistance (Ohms/phase)	36
Inductance (mH/phase)	28
Holding Torque (gf • cm)	1100
Detent Torque (gf • cm)	160
Rotor Inertia (g • cm ²)	23.7
Weight (kg)	0.25
Insulation Class	E
Ambient Temperature (°C)	-10 – 45
Temperature Rise (degrees)	70
Lead Specification	AWG #22

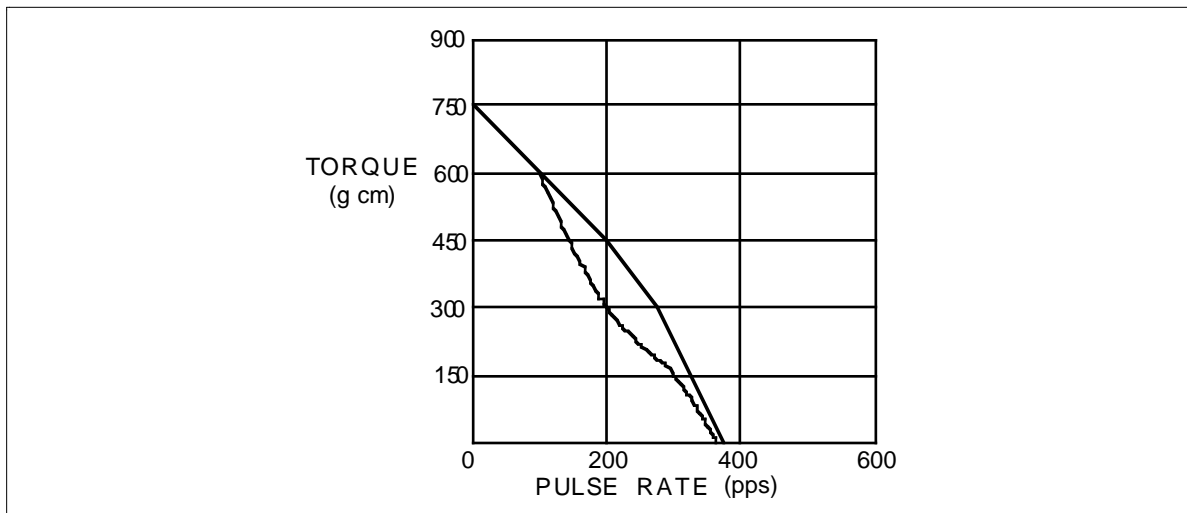


Figure 11

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