

DESIGN SHOWCASE

Load-Disconnect Switch Consumes Only 8 μ A

Deep discharge can damage a rechargeable battery. The **Figure 1** circuit, by disconnecting the battery from its load, halts battery discharge at a predetermined level of declining terminal voltage. Transistor Q_1 acts as the switch. The overall circuit draws about 500 μ A when the switch is closed and about 8 μ A when the switch is open.

Choosing the upper and lower voltage thresholds V_U and V_L lets you set values for R_1 , R_2 , and R_3 :

$$R_1 = R_2 * [(V_L / 1.15) - 1],$$

$$R_3 = 1.15 * R_1 / (V_U - V_L).$$

To start the circuit, battery voltage (V_+) must exceed V_U . The micropower voltage detector IC_1 then powers IC_2 , but only while V_+ remains above V_L . Otherwise, the loss of power to IC_2 removes gate drive from Q_1 , turning it off. As shown, the circuit disconnects a 3-cell nickel-cadmium battery from its load when V_+ reaches a V_L of 3.1V. An approximate 0.5V hysteresis prevents the switch from turning on immediately when the load is removed; V_+ must first return to V_U (3.6V).

IC_2 is a dual charge-pump inverter that normally converts 5V to 10V. The capacitors C_2 , C_3 , and two diodes on the chip's positive-voltage side form a voltage tripler that generates an approximate $2(V_+)$ gate drive for the high-side, floating-source MOSFET switch Q_1 .

Gate drive declines with battery voltage, causing the on-resistance of Q_1 to reach a maximum of $\approx 0.1\Omega$

just before V_+ reaches its 3.1V threshold. A 300mA load current at that time will cause a 30mV drop at the disconnect switch; the drop will be 2 to 3mV less for higher battery voltages. Resistor R_4 assures turn-off for Q_1 by providing a discharge path for C_3 .

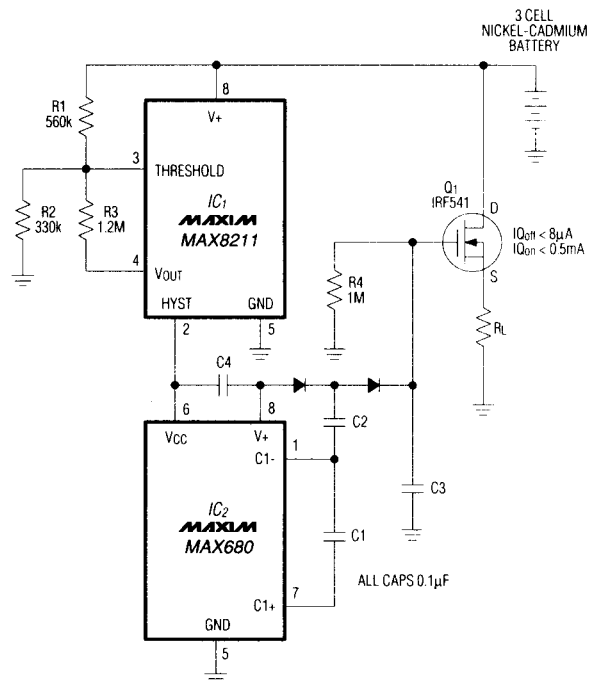


Figure 1. When battery voltage drops below a threshold set by R_1 and R_2 , the voltage-detector chip (IC_1) removes power from the charge pump IC_2 , which turns off the high-side switch Q_1 by removing its gate drive.

(Circle 3)