National Semiconductor

December 1994

LPC662
Low Power CMOS Dual Operational Amplifier

General Description

The LPC662 CMOS Dual operational amplifier is ideal for operation from a single supply. It features a wide range of operating voltage from +5V to +15V, rail-to-rail output swing in addition to an input common-mode range that includes ground. Performance limitations that have plagued CMOS amplifiers in the past are not a problem with this design. Input V_{OS}, drift, and broadband noise as well as voltage gain (into 100 kΩ and 5 kΩ) are all equal to or better than widely accepted bipolar equivalents, while the power supply requirement is typically less than 0.5 mW.

This chip is built with National's advanced Double-Poly Silicon-Gate CMOS process.

See the LPC660 datasheet for a Quad CMOS operational amplifier and LPC661 for a single CMOS operational amplifier with these same features.

Applications

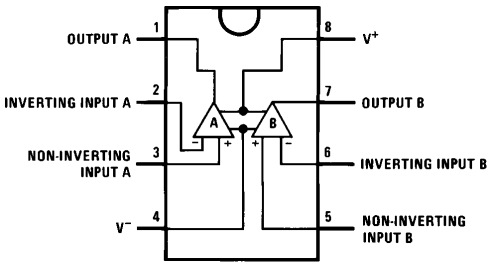
- High-impedance buffer
- Precision current-to-voltage converter
- Long-term integrator
- High-impedance preamplifier
- Active filter
- Sample-and-Hold circuit
- Peak detector

Features

- Rail-to-rail output swing
- Micropower operation (<0.5 mW)
- Specified for 100 kΩ and 5 kΩ loads
- High voltage gain 120 dB
- Low input offset voltage 3 mV
- Low offset voltage drift 1.3 μV/°C
- Ultra low input bias current 2 fA
- Input common-mode includes GND
- Operating range from +5V to +15V
- Low distortion 0.01% at 1 kHz
- Slew rate 0.11 V/μs
- Full military temperature range available

Connection Diagram

8-Pin DIP/SO



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Top View

Ordering Information

Package	Temperature Range		NSC Drawing	Transport Media
	Military	Industrial		
8-Pin Side Brazed Ceramic DIP	LPC662AMD		D08C	Rail
8-Pin Small Outline		LPC662AIM or LPC662IM	M08A	Rail Tape and Reel
8-Pin Molded DIP		LPC662AIN or LPC662IN	N08E	Rail
8-Pin Ceramic DIP	LPC662AMJ/883		J08A	Rail

RRD-B30M75/Printed in U. S. A.

Absolute Maximum Ratings (Note 3)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Differential Input Voltage	±Supply Voltage
Supply Voltage ($V^+ - V^-$)	16V
Output Short Circuit to V^+	(Note 11)
Output Short Circuit to V^-	(Note 1)
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temp. Range	−65°C to +150°C
Junction Temperature	150°C
ESD Rating (C = 100 pF, R = 1.5 kΩ)	1000V
Power Dissipation	(Note 2)
Current at Input Pin	±5 mA
Current at Output Pin	±18 mA
Current at Power Supply Pin	35 mA
Voltage at Input/Output Pin	$(V^+) + 0.3V$, $(V^-) - 0.3V$

Operating Ratings (Note 3)

Temperature Range	
LPC662AMJ/883	$-55°C \le T_J \le +125°C$
LPC662AM	$-55°C \le T_J \le +125°C$
LPC662AI	$-40°C \le T_J \le +85°C$
LPC662I	$-40°C \le T_J \le +85°C$
Supply Range	4.75V to 15.5V
Power Dissipation	(Note 9)
Thermal Resistance (θ_{JA}) (Note 10)	
8-Pin Ceramic DIP	100°C/W
8-Pin Molded DIP	101°C/W
8-Pin SO	165°C/W
8-Pin Side Brazed Ceramic DIP	100°C/W

DC Electrical Characteristics

Unless otherwise specified, all limits guaranteed for $T_J = 25°C$. **Boldface** limits apply at the temperature extremes. $V^+ = 5V$, $V^- = 0V$, $V_{CM} = 1.5V$, $V_O = 2.5V$ and $R_L > 1M$ unless otherwise specified.

Parameter	Conditions	Typ	LPC662AM LPC662AMJ/883 Limit (Notes 4, 8)	LPC662AI Limit (Note 4)	LPC662I Limit (Note 4)	Units
Input Offset Voltage		1	3	3	6	mV
			3.5	**3.3**	**6.3**	max
Input Offset Voltage Average Drift		1.3				μV/°C
Input Bias Current		0.002	20			pA
			100	**4**	**4**	max
Input Offset Current		0.001	20			pA
			100	**2**	**2**	max
Input Resistance		>1				Tera Ω
Common Mode Rejection Ratio	$0V \le V_{CM} \le 12.0V$, $V^+ = 15V$	83	70	70	63	dB
			68	**68**	**61**	min
Positive Power Supply Rejection Ratio	$5V \le V^+ \le 15V$, $V_O = 2.5V$	83	70	70	63	dB
			68	**68**	**61**	min
Negative Power Supply Rejection Ratio	$0V \le V^- \le -10V$	94	84	84	74	dB
			82	**83**	**73**	min
Input Common-Mode Voltage Range	$V^+ = 5V$ and 15V, For CMRR ≥ 50 dB	−0.4	−0.1	−0.1	−0.1	V
			0	**0**	**0**	max
		$V^+ - 1.9$	$V^+ - 2.3$	$V^+ - 2.3$	$V^+ - 2.3$	V
			$\mathbf{V^+ - 2.6}$	$\mathbf{V^+ - 2.5}$	$\mathbf{V^+ - 2.5}$	min

DC Electrical Characteristics

Unless otherwise specified, all limits guaranteed for $T_J = 25°C$. **Boldface** limits apply at the temperature extremes. $V^+ = 5V$, $V^- = 0V$, $V_{CM} = 1.5V$, $V_O = 2.5V$ and $R_L > 1M$ unless otherwise specified. (Continued)

Parameter	Conditions	Typ	LPC662AM LPC662AMJ/883 Limit (Notes 4, 8)	LPC662AI Limit (Note 4)	LPC662I Limit (Note 4)	Units
Large Signal Voltage Gain	$R_L = 100\ k\Omega$ (Note 5) Sourcing	1000	400	400	300	V/mV min
			250	**300**	**200**	
	Sinking	500	180	180	90	V/mV min
			70	**120**	**70**	
	$R_L = 5\ k\Omega$ (Note 5) Sourcing	1000	200	200	100	V/mV min
			150	**160**	**80**	
	Sinking	250	100	100	50	V/mV min
			35	**60**	**40**	
Output Swing	$V^+ = 5V$ $R_L = 100\ k\Omega$ to $V^+/2$	4.987	4.970	4.970	4.940	V min
			4.950	**4.950**	**4.910**	
		0.004	0.030	0.030	0.060	V max
			0.050	**0.050**	**0.090**	
	$V^+ = 5V$ $R_L = 5\ k\Omega$ to $V^+/2$	4.940	4.850	4.850	4.750	V min
			4.750	**4.750**	**4.650**	
		0.040	0.150	0.150	0.250	V max
			0.250	**0.250**	**0.350**	
	$V^+ = 15V$ $R_L = 100\ k\Omega$ to $V^+/2$	14.970	14.920	14.920	14.880	V min
			14.880	**14.880**	**14.820**	
		0.007	0.030	0.030	0.060	V max
			0.050	**0.050**	**0.090**	
	$V^+ = 15V$ $R_L = 5\ k\Omega$ to $V^+/2$	14.840	14.680	14.680	14.580	V min
			14.600	**14.600**	**14.480**	
		0.110	0.220	0.220	0.320	V max
			0.300	**0.300**	**0.400**	
Output Current $V^+ = 5V$	Sourcing, $V_O = 0V$	22	16	16	13	mA min
			12	**14**	**11**	
	Sinking, $V_O = 5V$	21	16	16	13	mA min
			12	**14**	**11**	
Output Current $V^+ = 15V$	Sourcing, $V_O = 0V$	40	19	28	23	mA min
			19	**25**	**20**	
	Sinking, $V_O = 13V$ (Note 11)	39	19	28	23	mA min
			19	**24**	**19**	
Supply Current	Both Amplifiers $V_O = 1.5V$	86	120	120	140	μA max
			145	**140**	**160**	

AC Electrical Characteristics

Unless otherwise specified, all limits guaranteed for $T_J = 25°C$. **Boldface** limits apply at the temperature extremes. $V^+ = 5V$, $V^- = 0V$, $V_{CM} = 1.5V$, $V_O = 2.5V$ and $R_L > 1M$ unless otherwise specified.

Parameter	Conditions	Typ	LPC662AM LPC662AMJ/883 Limit (Notes 4, 8)	LPC662AI Limit (Note 4)	LPC662I Limit (Note 4)	Units
Slew Rate	(Note 6)	0.11	0.07	0.07	0.05	V/μs min
			0.04	**0.05**	**0.03**	
Gain-Bandwidth Product		0.35				MHz
Phase Margin		50				Deg
Gain Margin		17				dB
Amp-to-Amp Isolation	(Note 7)	130				dB
Input Referred Voltage Noise	F = 1 kHz	42				nV/$\sqrt{Hz}$
Input Referred Current Noise	F = 1 kHz	0.0002				pA/$\sqrt{Hz}$
Total Harmonic Distortion	F = 1 kHz, $A_V = -10$, $V^+ = 15V$ $R_L = 100\ k\Omega$, $V_O = 8\ V_{PP}$	0.01				%

Note 1: Applies to both single supply and split supply operation. Continuous short circuit operation at elevated ambient temperature and/or multiple Op Amp shorts can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversely affect reliability.

Note 2: The maximum power dissipation is a function of $T_{J(max)}$, θ_{JA}, and T_A. The maximum allowable power dissipation of any ambient temperature is $P_D = (T_{J(max)} - T_A)/\theta_{JA}$.

Note 3: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.

Note 4: Limits are guaranteed by testing or correlation.

Note 5: $V^+ = 15V$, $V_{CM} = 7.5V$ and R_L connected to 7.5V. For Sourcing tests, $7.5V \le V_O \le 11.5V$. For Sinking tests, $2.5V \le V_O \le 7.5V$.

Note 6: $V^+ = 15V$. Connected as Voltage Follower with 10V step input. Number specified is the slower of the positive and negative slew rates.

Note 7: Input referred. $V^+ = 15V$ and $R_L = 100\ k\Omega$ connected to $V^+/2$. Each amp excited in turn with 1 kHz to produce $V_O = 13\ V_{PP}$.

Note 8: A military RETS electrical test specification is available on request. At the time of printing, the LPC662AMJ/883 RETS specification complied fully with the **boldface** limits in this column. The LPC662AMJ/883 may also be procured to a Standard Military Drawing specification.

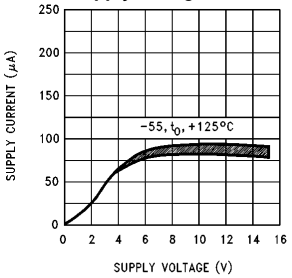
Note 9: For operating at elevated temperatures the device must be derated based on the thermal resistance θ_{JA} with $P_D = (T_J - T_A)/\theta_{JA}$.

Note 10: All numbers apply for packages soldered directly into a PC board.

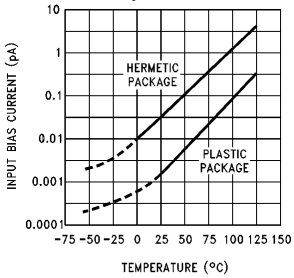
Note 11: Do not connect output to V^+ when V^+ is greater than 13V or reliability may be adversely affected.

Typical Performance Characteristics $V_S = \pm 7.5V$, $T_A = 25°C$ unless otherwise specified

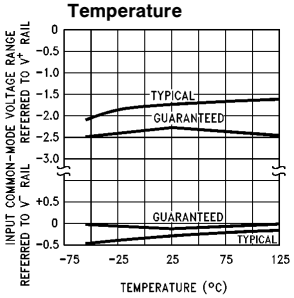
Supply Current vs Supply Voltage



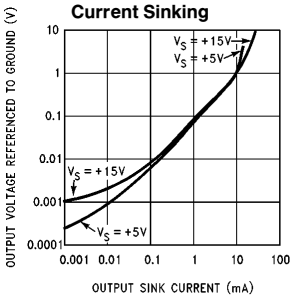
Input Bias Current vs Temperature



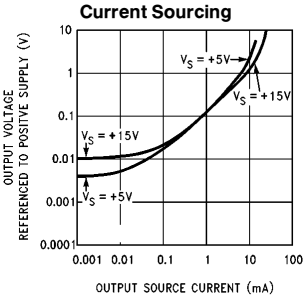
Input Common-Mode Voltage Range vs Temperature



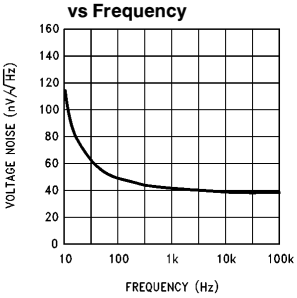
Output Characteristics Current Sinking



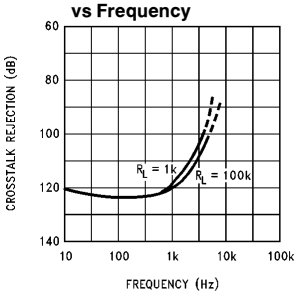
Output Characteristics Current Sourcing



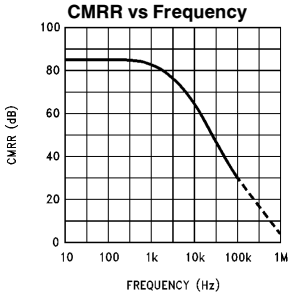
Input Voltage Noise vs Frequency



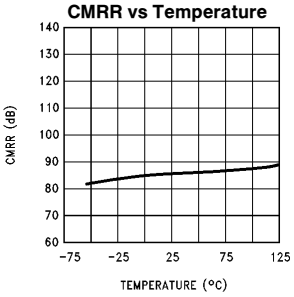
Crosstalk Rejection vs Frequency



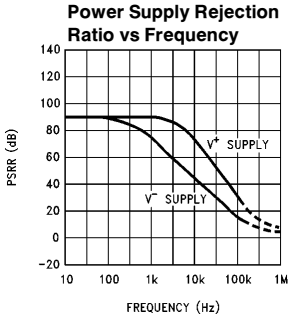
CMRR vs Frequency



CMRR vs Temperature



Power Supply Rejection Ratio vs Frequency



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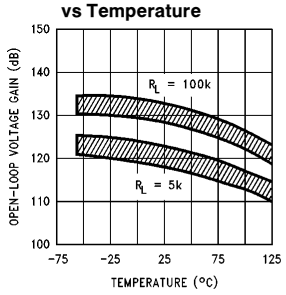
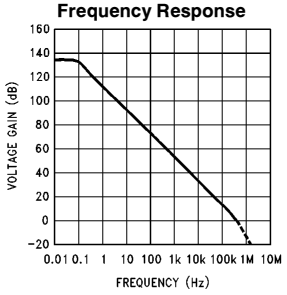
Typical Performance Characteristics $V_S = \pm 7.5V$, $T_A = 25°C$ unless otherwise specified (Continued)

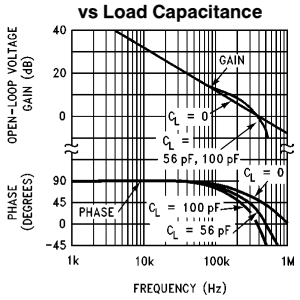
Open-Loop Voltage Gain vs Temperature



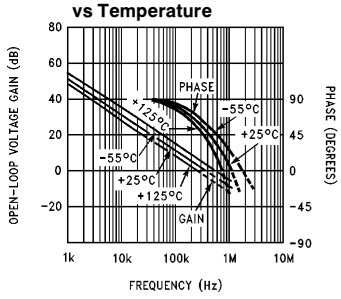
Open-Loop Frequency Response



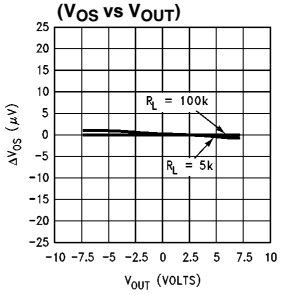
Gain and Phase Responses vs Load Capacitance



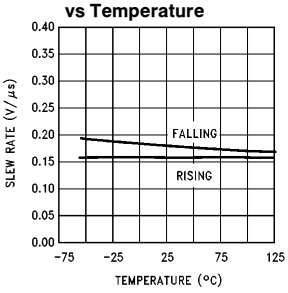
Gain and Phase Responses vs Temperature



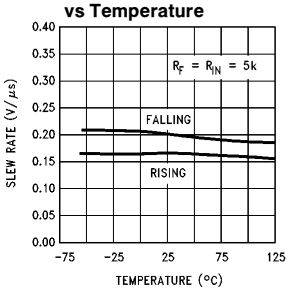
Gain Error (V_{OS} vs V_{OUT})



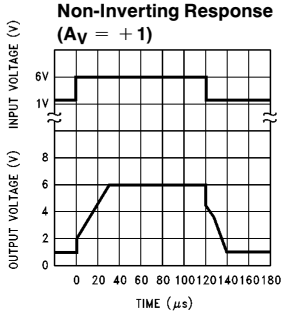
Non-Inverting Slew Rate vs Temperature



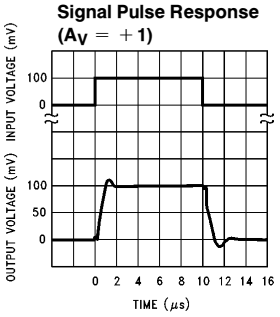
Inverting Slew Rate vs Temperature



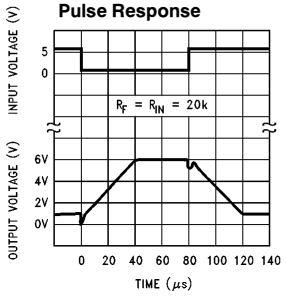
Large-Signal Pulse Non-Inverting Response ($A_V = +1$)



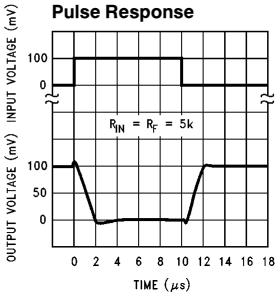
Non-Inverting Small Signal Pulse Response ($A_V = +1$)



Inverting Large-Signal Pulse Response



Inverting Small-Signal Pulse Response



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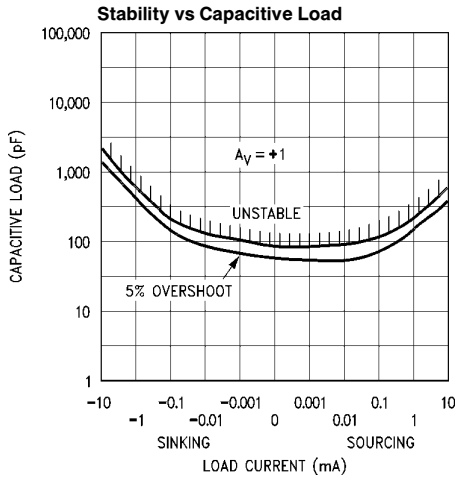
Typical Performance Characteristics $V_S = \pm 7.5V$, $T_A = 25°C$ (Continued)



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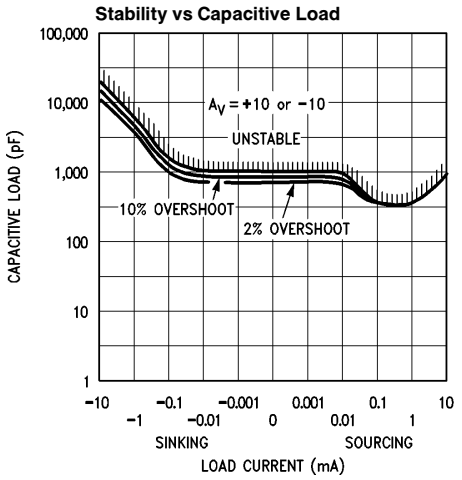

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Note: Avoid resistive loads of less than 500Ω, as they may cause instability.

Application Hints

AMPLIFIER TOPOLOGY

The topology chosen for the LPC662 is unconventional (compared to general-purpose op amps) in that the traditional unity-gain buffer output stage is not used; instead, the output is taken directly from the output of the integrator, to allow rail-to-rail output swing. Since the buffer traditionally delivers the power to the load, while maintaining high op amp gain and stability, and must withstand shorts to either rail, these tasks now fall to the integrator.

As a result of these demands, the integrator is a compound affair with an embedded gain stage that is doubly fed forward (via C_f and C_{ff}) by a dedicated unity-gain compensation driver. In addition, the output portion of the integrator is a push-pull configuration for delivering heavy loads. While sinking current the whole amplifier path consists of three gain stages with one stage fed forward, whereas while sourcing the path contains four gain stages with two fed forward.

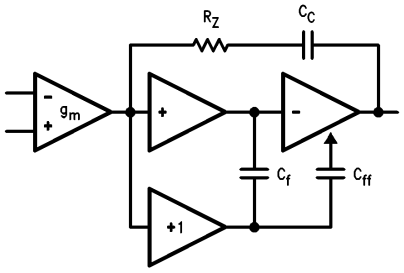

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FIGURE 1. LPC662 Circuit Topology (Each Amplifier)

The large signal voltage gain while sourcing is comparable to traditional bipolar op amps for load resistance of at least 5 kΩ. The gain while sinking is higher than most CMOS op amps, due to the additional gain stage; however, when driving load resistance of 5 kΩ or less, the gain will be reduced as indicated in the Electrical Characteristics. The op amp can drive load resistance as low as 500Ω without instability.

COMPENSATING INPUT CAPACITANCE

Refer to the LMC660 or LMC662 datasheets to determine whether or not a feedback capacitor will be necessary for compensation and what the value of that capacitor would be.

CAPACITIVE LOAD TOLERANCE

Like many other op amps, the LPC662 may oscillate when its applied load appears capacitive. The threshold of oscillation varies both with load and circuit gain. The configuration most sensitive to oscillation is a unity-gain follower. See the Typical Performance Characteristics.

The load capacitance interacts with the op amp's output resistance to create an additional pole. If this pole frequency is sufficiently low, it will degrade the op amp's phase margin so that the amplifier is no longer stable at low gains. The addition of a small resistor (50Ω to 100Ω) in series with the op amp's output, and a capacitor (5 pF to 10 pF) from inverting input to output pins, returns the phase margin to a safe value without interfering with lower-frequency circuit

Application Hints (Continued)

operation. Thus, larger values of capacitance can be tolerated without oscillation. Note that in all cases, the output will ring heavily when the load capacitance is near the threshold for oscillation.

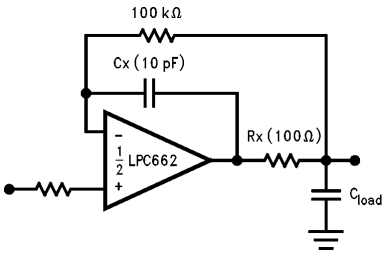

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FIGURE 2a. Rx, Cx Improve Capacitive Load Tolerance

Capacitive load driving capability is enhanced by using a pull up resistor to V^+ *(Figure 2b)*. Typically a pull up resistor conducting 50 μA or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the amplifier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see Electrical Characteristics).

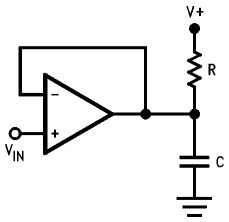

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FIGURE 2b. Compensating for Large Capacitive Loads with A Pull Up Resistor

PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low bias current of the LPC662, typically less than 0.04 pA, it is essential to have an excellent layout. Fortunately, the techniques for obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LPC662's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs. See *Figure 3*. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of 10^{12} ohms, which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of an input. This would cause a 100 times degradation from the LPC662's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of 10^{11} ohms would cause only 0.05 pA of leakage current, or perhaps a minor (2:1) degradation of the amplifier's performance. See *Figures 4a*, *4b*, *4c* for typical connections of guard rings for standard op-amp configurations. If both inputs are active and at high impedance, the guard can be tied to ground and still provide some protection; see *Figure 4d*.

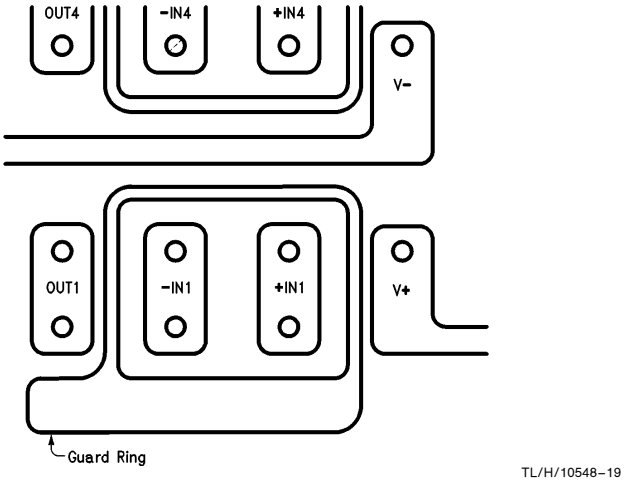

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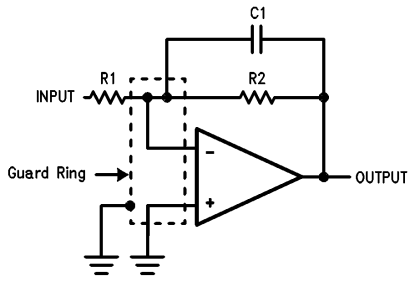
FIGURE 3. Example of Guard Ring in P.C. Board Layout, using the LPC660

Application Hints (Continued)



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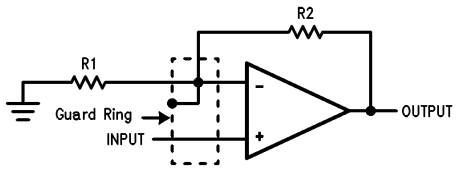
(a) Inverting Amplifier



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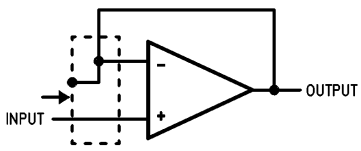
(b) Non-Inverting Amplifier



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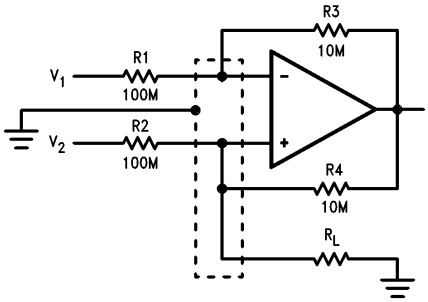
(c) Follower



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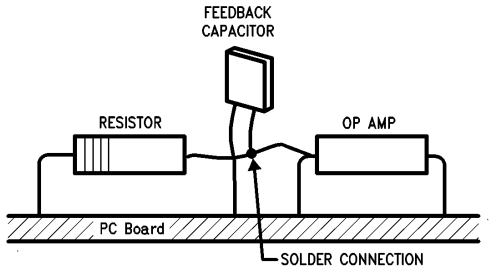
(d) Howland Current Pump

FIGURE 4. Guard Ring Connections

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See *Figure 5*.



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(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board.)

FIGURE 5. Air Wiring

BIAS CURRENT TESTING

The test method of *Figure 6* is appropriate for bench-testing bias current with reasonable accuracy. To understand its operation, first close switch S2 momentarily. When S2 is opened, then

$$I^- = \frac{dV_{OUT}}{dt} \times C2.$$

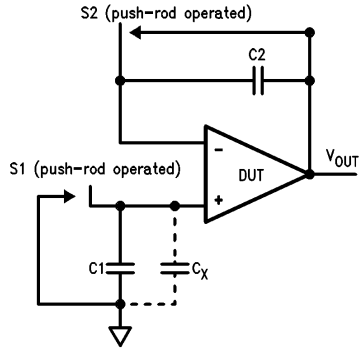

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FIGURE 6. Simple Input Bias Current Test Circuit

Application Hints (Continued)

A suitable capacitor for C2 would be a 5 pF or 10 pF silver mica, NPO ceramic, or air-dielectric. When determining the magnitude of I^-, the leakage of the capacitor and socket must be taken into account. Switch S2 should be left shorted most of the time, or else the dielectric absorption of the capacitor C2 could cause errors.

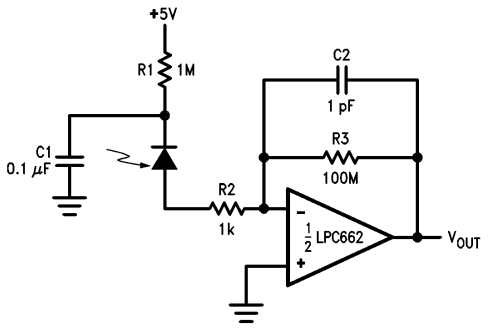
Similarly, if S1 is shorted momentarily (while leaving S2 shorted)

$$I^+ = \frac{dV_{OUT}}{dt} \times (C1 + C_X)$$

where C_X is the stray capacitance at the + input.

Typical Single-Supply Applications ($V^+ = 5.0\ V_{DC}$)

Photodiode Current-to-Voltage Converter



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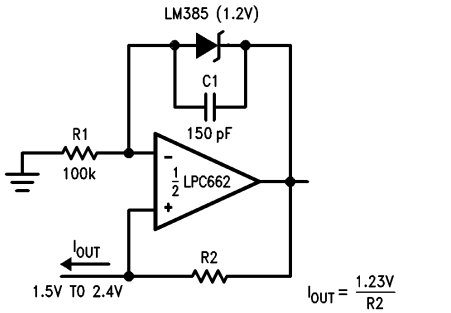
Note: A 5V bias on the photodiode can cut its capacitance by a factor of 2 or 3, leading to improved response and lower noise. However, this bias on the photodiode will cause photodiode leakage (also known as its dark current).

Micropower Current Source



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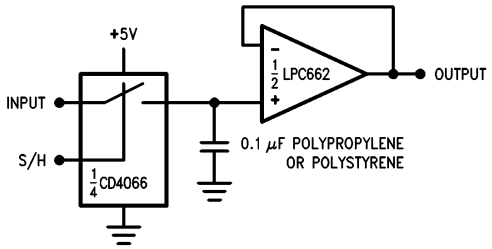
(Upper limit of output range dictated by input common-mode range; lower limit dictated by minimum current requirement of LM385.)

Low-Leakage Sample-and-Hold



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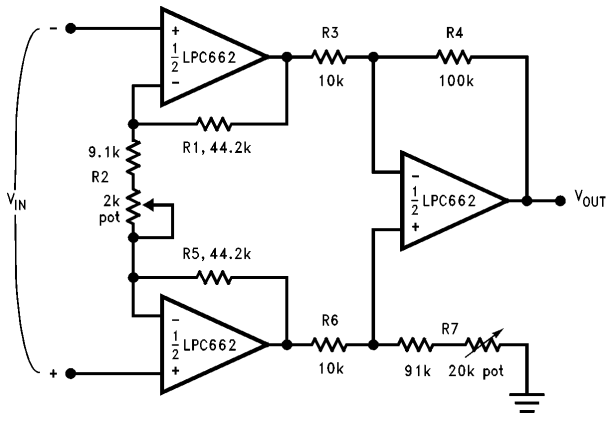
Instrumentation Amplifier



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If R1 = R5, R3 = R6 and R4 = R7; then

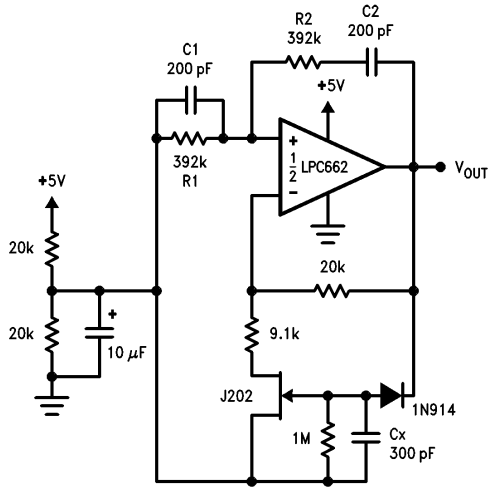
$$\frac{V_{OUT}}{V_{IN}} = \frac{R2 + 2R1}{R2} \times \frac{R4}{R3}$$

$\therefore A_V \approx 100$ for circuit shown.

For good CMRR over temperature, low drift resistors should be used. Matching of R3 to R6 and R4 to R7 affects CMRR. Gain may be adjusted through R2. CMRR may be adjusted through R7.

Typical Single-Supply Applications ($V^+ = 5.0\ V_{DC}$) (Continued)

Sine-Wave Oscillator



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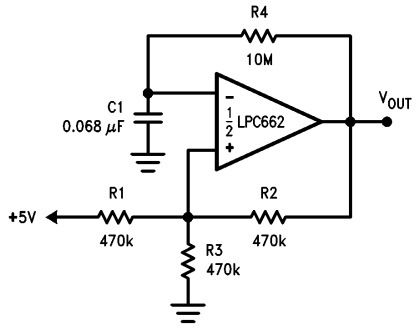
Oscillator frequency is determined by R1, R2, C1, and C2:

$$f_{OSC} = 1/2\pi RC$$

where R = R1 = R2 and C = C1 = C2.

This circuit, as shown, oscillates at 2.0 kHz with a peak-to-peak output swing of 4.5V

1 Hz Square-Wave Oscillator



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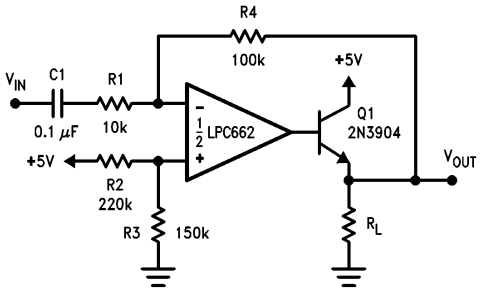
Power Amplifier



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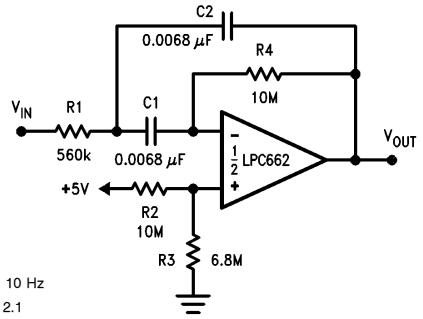
Typical Single-Supply Applications ($V^+ = 5.0\ V_{DC}$) (Continued)

10 Hz Bandpass Filter



$f_O = 10$ Hz
$Q = 2.1$
Gain $= -8.8$

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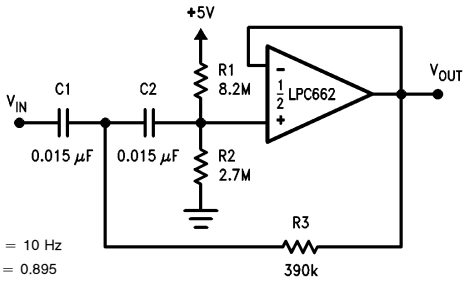
10 Hz High-Pass Filter (2 dB Dip)



$f_c = 10$ Hz
$d = 0.895$
Gain $= 1$

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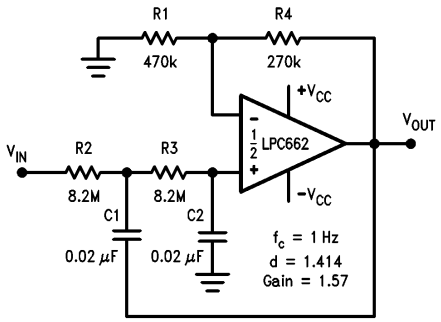
1 Hz Low-Pass Filter (Maximally Flat, Dual Supply Only)



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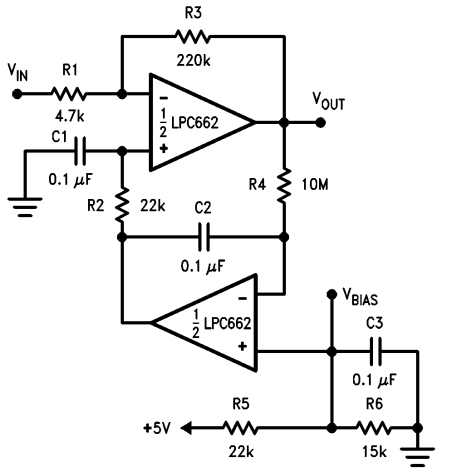
High Gain Amplifier with Offset Voltage Reduction



Gain $= -46.8$

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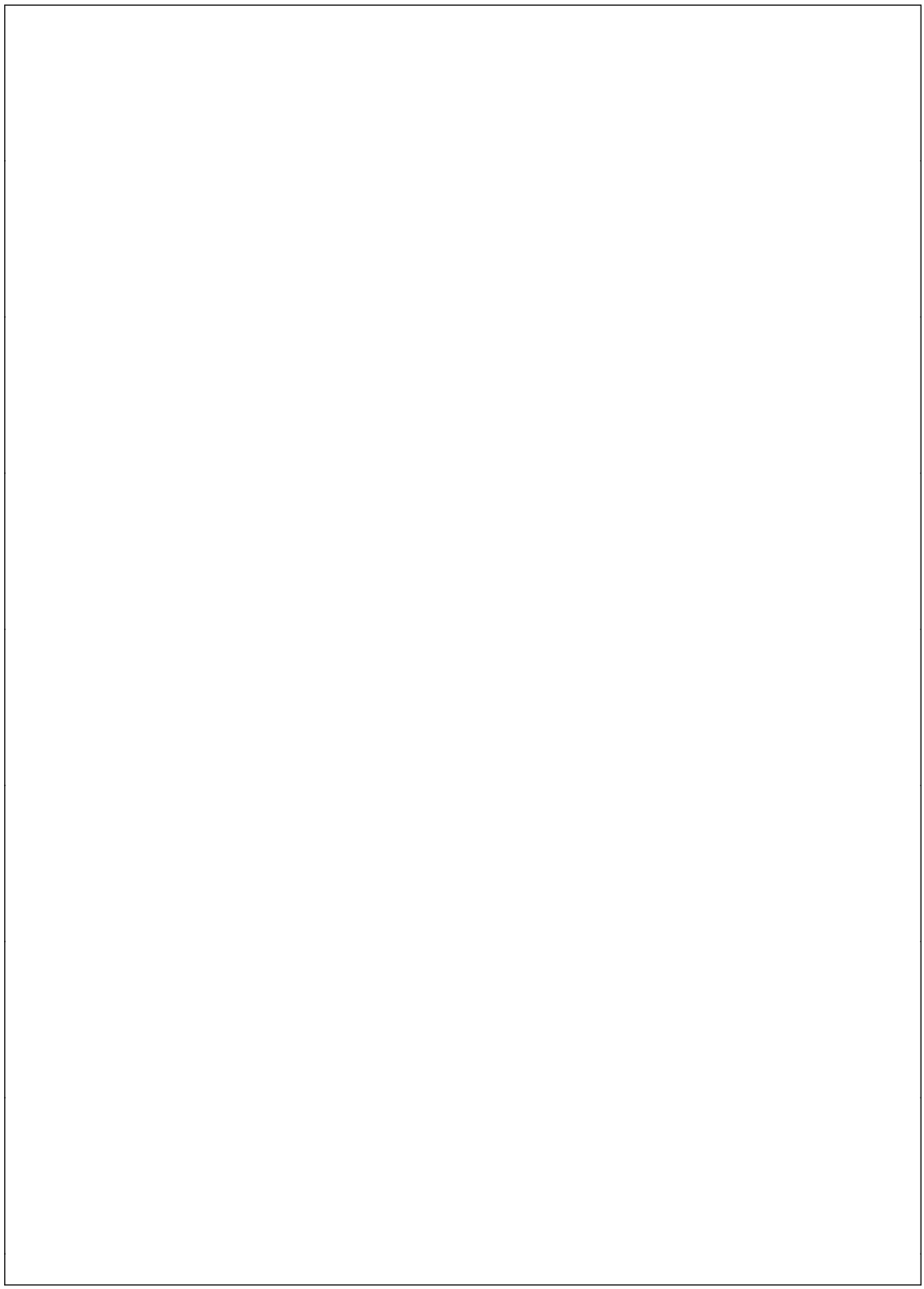
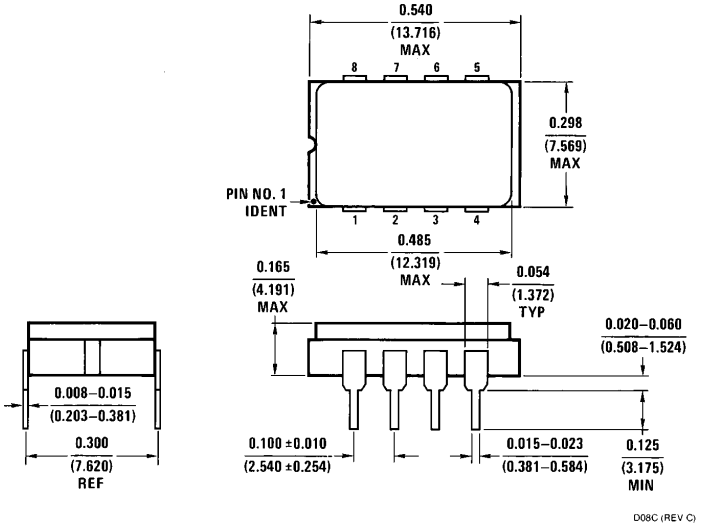
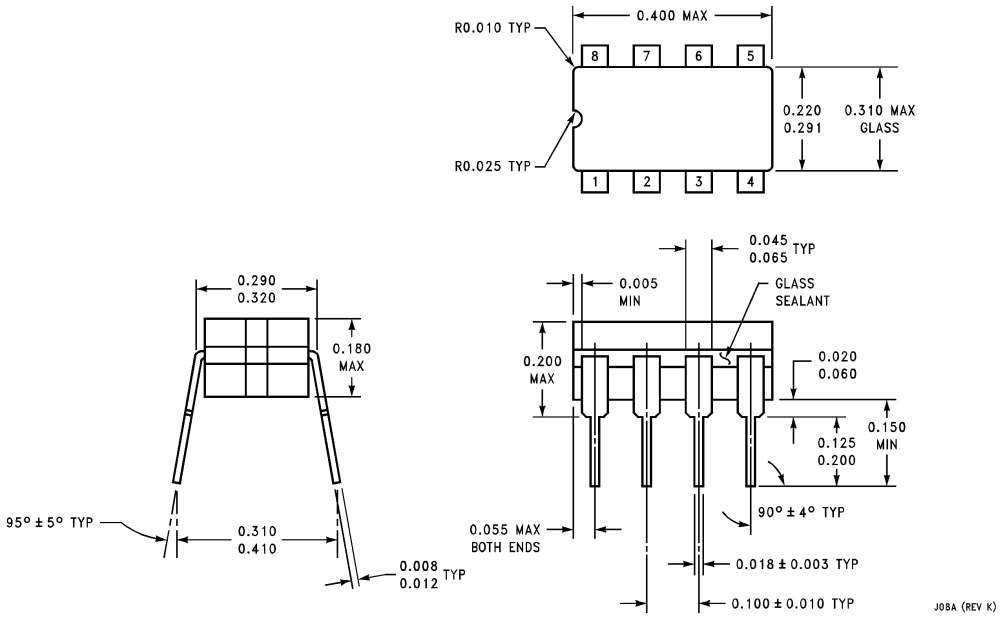
Output offset voltage reduced to the level of the input offset voltage of the bottom amplifier (typically 1 mV), referred to V_{BIAS}.



Physical Dimensions inches (millimeters)

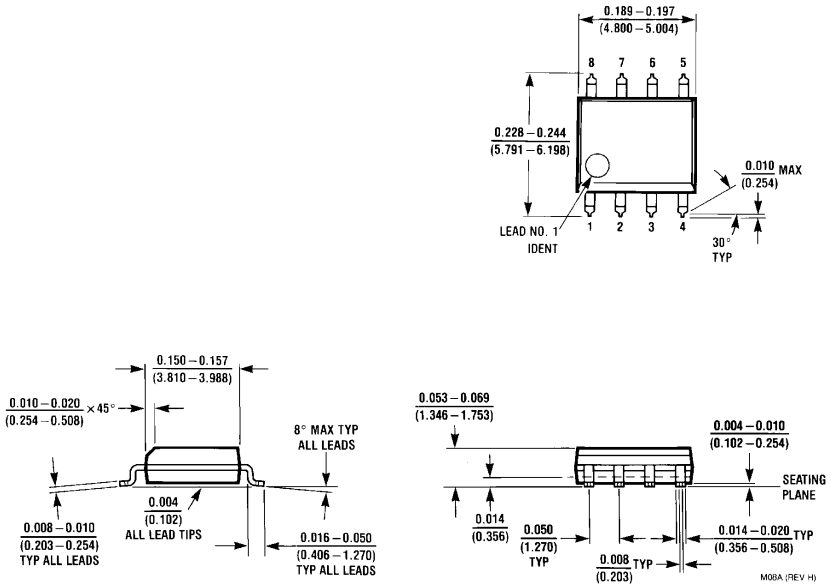


8-Pin Cavity Dual-In-Line Package (D)
Order Number LPC662AMD
NS Package Number D08C



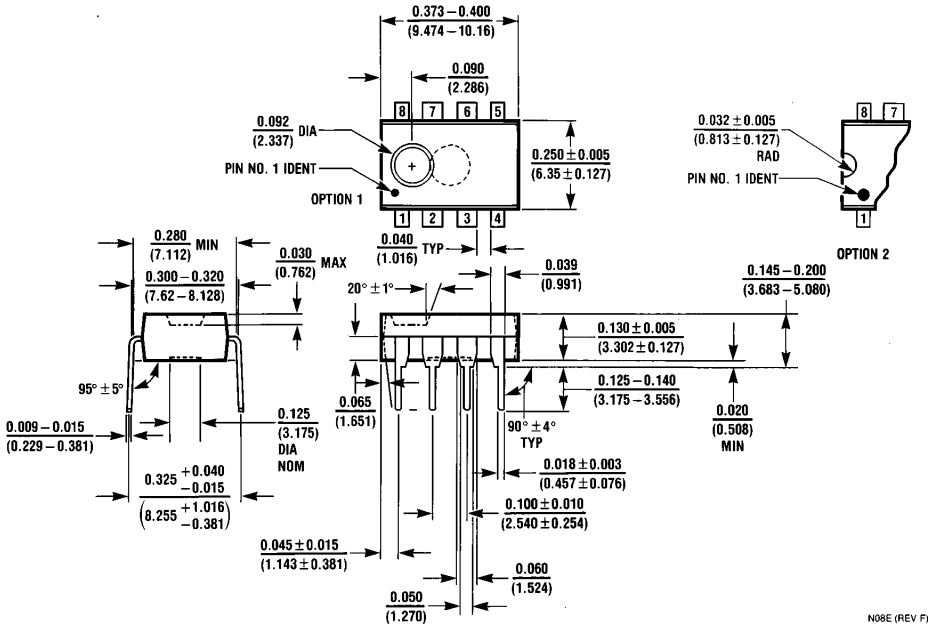
Ceramic Dual-In-Line Package (J)
Order Number LPC662AMJ/883
NS Package Number J08A

Physical Dimensions inches (millimeters) (Continued)



8-Pin Small Outline Molded Package (M)
Order Number LPC662AIM or LPC662IM
NS Package Number M08A

Physical Dimensions inches (millimeters) (Continued)



8-Pin Molded Dual-In-Line Package (N)
Order Number LPC662AIN or LPC662IN
NS Package Number N08E

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